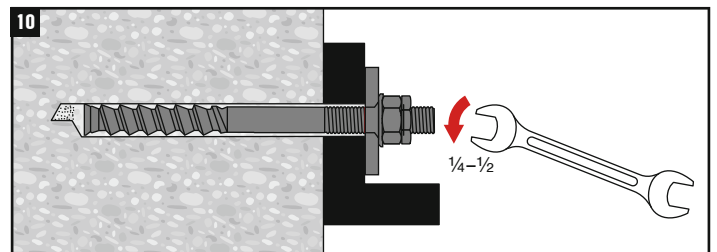
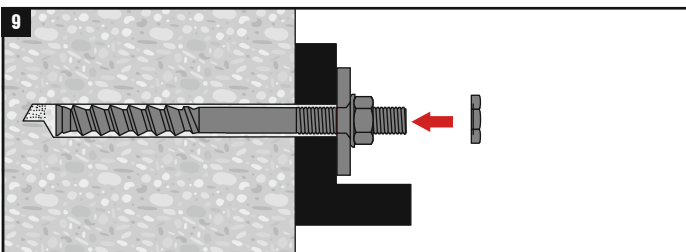
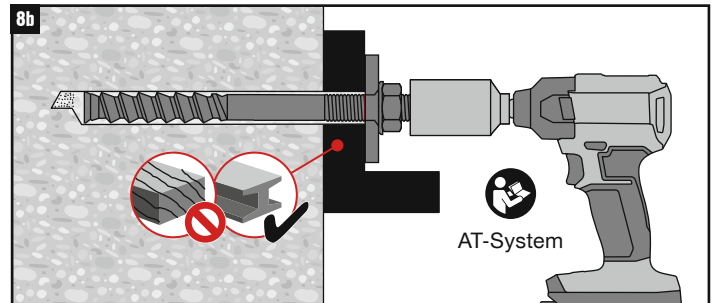
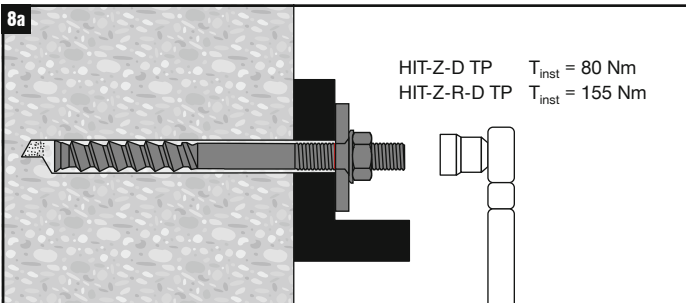
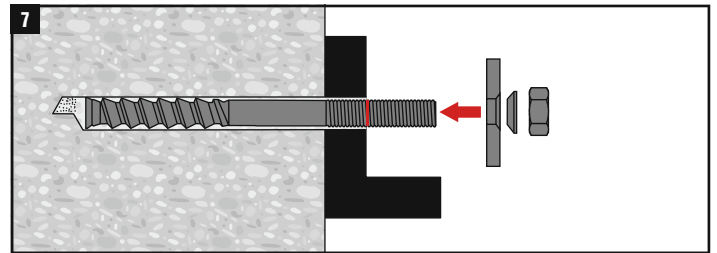
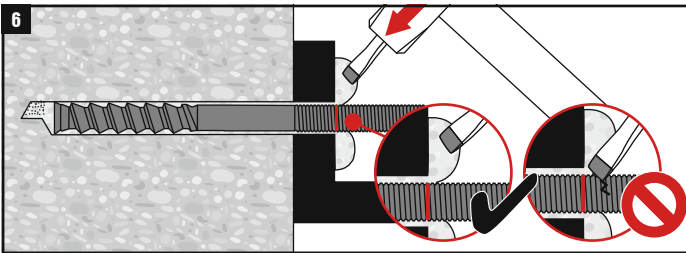
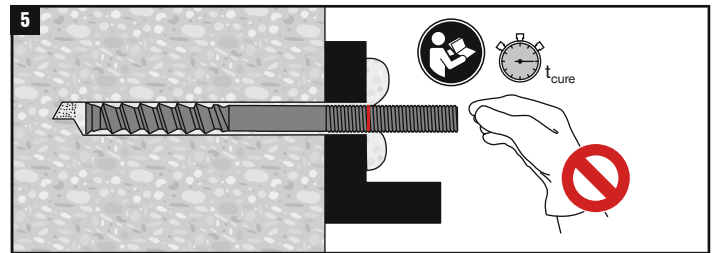
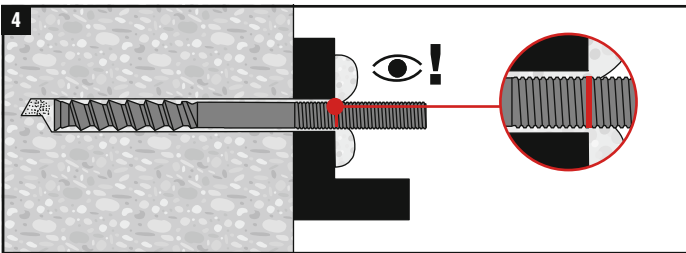
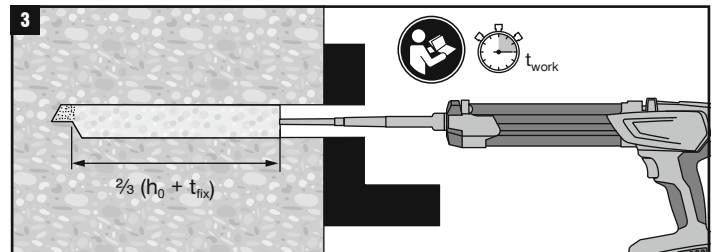
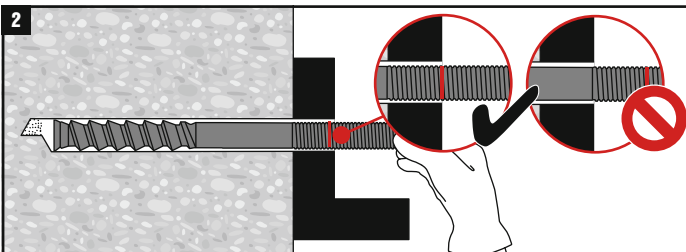
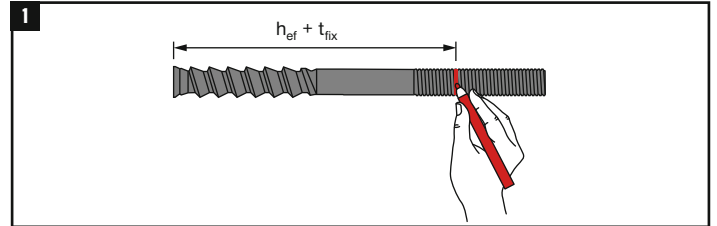
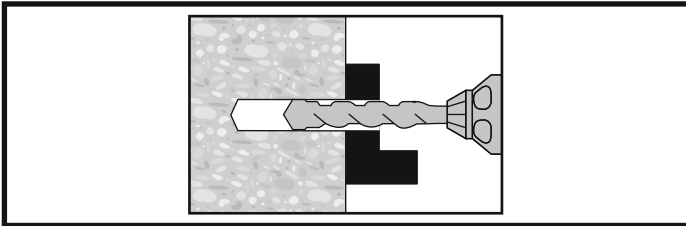
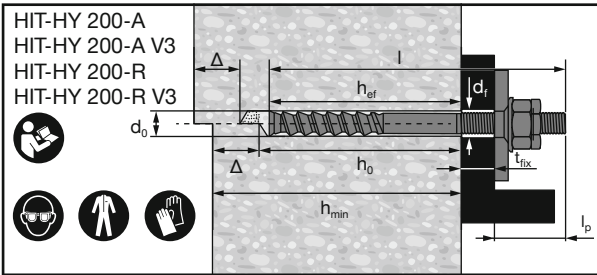


	d_0 [mm]	d_f [mm]	h_{ef} [mm]	l_p [mm]	Δ [mm]	h_{min} [mm]	t_{fix} [mm]	T_{inst} [mm]	SW [mm]	AT System
HIT-Z-D TP	18	20	125	≥ 35	$2 \times d_0$	160	$l - 160 \geq 10$	80	24	SIW 6AT-22
HIT-Z-R-D TP	18	20	125	≥ 35	$2 \times d_0$	160	$l - 160 \geq 10$	155	24	+ SI-AT-22

$+5^\circ \dots 40^\circ\text{C} / 41^\circ \dots 104^\circ\text{F}$





	d_0 [mm]	d_f [mm]	h_{ef} [mm]	l_p [mm]	Δ [mm]	h_{min} [mm]	t_{fix} [mm]	T_{inst} [mm]	SW [mm]	AT System
HIT-Z-D TP	18	20	125	≥ 35	$2 \times d_0$	160	$l - 160 \geq 10$	80	24	SIW 6AT-22
HIT-Z-R-D TP	18	20	125	≥ 35	$2 \times d_0$	160	$l - 160 \geq 10$	155	24	+ SI-AT-22

$+5^\circ \dots 40^\circ\text{C} / 41^\circ \dots 104^\circ\text{F}$

